# ADSORPTION OF COPPER ON SURFACES OF FEASIBLE MATERIALS (PLANT WASTE, SLUDGE AND BENTONITE) METAL)

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ABSTRACT		

Extraction of Copper ion from its water solutions using plant waste (compost), sludge and Bentonite metal as cheap natural adsorbed materials. It was found that Copper ion extraction was based on concentration of Copper and amount of the adsorbed materials. Highest amount of adsorption was obtained at 180  $\mu$ g Cu ml<sup>-1</sup> as Bentonite, plant waste and sludge respectively. Thermal equilibrium of the system was studied by Langmuir equation, R<sup>2</sup> gave a good linear relationship in succession. Maximum regulatory capacity and regulatory capacity at equilibrium is 1.0, 0.99 and 0.96 to plant waste, sludge and Bentonite respectively, as the preference coefficient constant calculated by the Langmuir equation indicate that adsorption is preferable and irriversible for plant waste and sludge while not preferentially and reversible for bentonite.  $\Delta G$  adsorption reactions were automatic for the Bentonite metal, while for plant waste and sludge non-spontaneous reaction and needs extra activation energy. It is clear from the above that the use of natural materials in the extraction of copper ion is a very effective method and it is an inexpensive and friendly methods envirooment.

Keywords : preference coefficient,  $\Delta G$  for adsorption reactions, natural adsorbents.

الحياني واخرون	659-654:(3)5	مجلة العلوم الزراعية العراقية -2022 : 33
أة ومعدن البنتونايت)	سطوح مواد رخيصة الثمن (مخلفات نباتية والحم	امتزاز النحاس على
محمد علي جمال العبيدي	سميرة ناصر حسون الحسون	عبد الستار جبير زبن الحياني
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قسم علوم التربة والموارد المائية	الزراعية / قسم علوم التربة والموارد المائية	وتقاناتها، قسم تقانات البيئة
		المستخلص

تم دراسة استخلاص أيون النحاس من محاليله المائية باستخدام مخلفات النباتات (كمبوست) والحمأة ومعدن البنتونايت كمادة مازة طبيعية رخيصة الثمن. وجد أن استخلاص أيون النحاس يعتمد على تركيز أيون النحاس وكمية المادة المازة ، إذ تم الحصول على أعلى كمية إمتزاز عند التركيز 180 مايكروغرام Cu مل <sup>-1</sup> مع استخدام معدن البنتونايت ثم المخلفات النباتية ثم الحصول على أعلى كمية إمتزاز عند التركيز 180 مايكروغرام Cu مل <sup>-1</sup> مع استخدام معدن البنتونايت ثم المخلفات النباتية ثم المحماة. تم الحصول على أعلى كمية المارة التركيز 180 مايكروغرام Cu مل <sup>-1</sup> مع استخدام معدن البنتونايت ثم المخلفات النباتية ثم الحماة. تم دراسة الاتزان الحراري للنظام باستخدام معادلة لانجماير ، إذ أعطى النظام معامل تحديد (<sup>R</sup>) علاقة خطية جيدة بلغ 1 و 0.90 و 0.96 للمخلفات النباتية والحمأة ومعدن البنتونايت بالتتابع مما يدل على ملائمة النموذج للنظام تحت الدراسة. إذ أيشير ثابت معامل التفضيل المحسوب بواسطة معادلة لانجماير إلى أن الإمتزاز يكون مفضلاً وغير عكسي بالنسبة الدراسة. إذ يشير ثابت معامل التفضيل المحسوب بواسطة معادلة لانجماير إلى أن الإمتزاز يكون مفضلاً وغير عكسي بالنسبة المخلفات النباتية والحمأة ومعدن البنتونايت بالت المعروس. كان معامل التفضيل المحسوب بواسطة معادلة لانجماير إلى أن الإمتزاز يكون مفضلاً وغير عكسي بالنسبة المزاسة. إذ يشير ثابت معامل التفضيل المحسوب بواسطة معادلة لانجماير إلى أن الإمتزاز يكون مفضلاً وغير عكسي بالنسبة المخلفات النباتات والحمأة بينما غير مفضل وعكسي للبنتونايت ، للنظام المدروس. كانت الطاقة الحرة (Δα) لتفاعلات المخلفات النباتات والحمأة بينما غير مفضل وعكسي للبنتونايت ، للنظام المدروس. كانت الطاقة الحرة (Δα) لتفاعلات المخلفات النبات والحمأة غير تلفائية وتحتاج إلى طاقة تنشيط إضافية. الإمتزاز لمعدن البنتونايت تلفائية ، بينما كانت تفاعلات المخلفات النبات والحمأة غير ملوقة فعالة وتحتاج إلى طاقة تنشيط إضافية. مما سبق يتضح أن استخدام مواد مازة طبيعية في استخلاص أيون النحاس تعد طريقة فعالة جدا ، ومن مميزاته أنه يعتبر من الطرق غير المكلفة والصديقة للبيئة.

الكلمات المفتاحية: معامل التفضيل، الطاقة الحرة لتفاعلات الإمتزاز (ΔG)، المواد المازة الطبيعية

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## **INTRODUCTION**

Water pollution caused by industrial and human activities is considered as one of the major problems in the world, as it is the leading cause of 80% of diseases worldwide (7), and due to United Nations Organization reports, there is almost 1.1 billion people that can not get potible water mostly from poor and developing countries (1). There are thousands of chemical compounds that are discharged daily directly or indirectly to water sources without any treatment (16). Among these substances are the most dangerous and harmful heavy metals, even when present and in low concentrations, because they accumulate inside living tissues (14,17). Some heavy metals such as Iron, Copper and Zinc are necessary to maintain vital activities in living organisms, while Others, such as Lead and Cadmium, play no role in these activities and are therefore classified as toxic elements, but at high concentrations, all heavy elements, whether necessary or unnecessary, cause toxicity to organisms (6). There are many methods used to remove heavy metals such as chemical deposition, membrane separation, ion exchange, liquid extraction, electrodialysis, and adsorption (15,18, 10). The use of powders such as activated Carbon, Silica, Т

Alumina, etc., is excellent in removing heavy but costly elements and their manufacturing process is accompanied by the production of environmental pollutants, leading to the use of alternative materials (natural powders) that are available in large quantities or unused or present in wastes (13,19). Therefore, much research is conducted on various types of natural materials that have proven to be effective in extracting heavy metals (Bentonite and Silicate clay minerals) and many organic materials (3,4,5,11). The use of plant residues (compost), sludge and Bentonite is considered a natural mezzanine, as it is a cheap material for the recovery of heavy metals, including Copper ion. To this end, plant residues (compost), sludge and bentonite were used to study their ability to extract this ion from their aqueous solutions as a method used to treat copper-contaminated water and solutions and to determine the maximum adsorption capacity and binding capacity of the adsorbed ion.=

# MATERIALS AND METHODS Preparation of the material

Plant waste (compost), sludge and Bentonite were used as natural adsorbents as their properties are listed in tables 1 and 2.

environmental media		pH	EC			(	%			
		itur meuru	P	dS m <sup>-1</sup>	V	Vater holdi	ng capacity	N	Р	K
P	lant waste	(compost)	7.2	4.8		680		1.44	0.31	0.97
	Sludge		7.9	1.8		140		0.98	1.36	0.52
			Table	2 . Metal	l compo	osition of	Bentonite	<u>,</u>		
Total	L.O.I	Fe <sub>2</sub> O <sub>3</sub>	Na <sub>2</sub> O	K <sub>2</sub> O	MgO	CaO	Al <sub>2</sub> O <sub>3</sub>	SiO <sub>2</sub>	constituent	
99.66	12.49	5.12	1.11	0.60	3.42	4.48	15.67	56.77	% W	

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Fabla 1	Somo	chemical	nron	orting	Λť	como	onvire	nmontol	modia
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## **Chemical treatment**

Media samples (plant waste, sludge and bentonite) were taken, dried, grinded, passed through a sieve of 2 mm opening diameter, a mass of 2 g was taken from each sample, and placed in a 50 cm<sup>3</sup> centrifuge tube and 6 copper nitrate levels added (Cu(NO<sub>3</sub>)<sub>2</sub>.3H<sub>2</sub>O) are 60, 80, 100, 120, 140 and 180, at a ratio of 1: 10 (the volume of the added solution 20 cm<sup>3</sup>) and with three replicates, (copper concentrations were prepared using 0.03 standard of calcium nitrate (Ca (NO<sub>3</sub>)<sub>2</sub>.4H<sub>2</sub>O), as an electrolytic solution to reduce changes in Ionic strength). The tubes were shaken by an

electric shaker for 6 hours at 25°C. The balanced solution was separated from the centrifuge precipitator at a speed of 3000 rp m<sup>-1</sup> for 10 minutes. The concentration of copper in 10 cm<sup>3</sup> of the equilibrium solution was determined by using an atomic absorption device( $C_{in}$ , and final concentration ( $C_{fin}$ , µg ml<sup>-1</sup>), in each flask

$$Cu^{2+} - ad. = \frac{V(C_{in} - C_{fin})}{W} ... (1)$$

Where:

 $Cu^{2+}$ -ad. : Amount of copper adsorbed in  $\mu g$  g<sup>-1</sup>, V: volume of copper solution in flask in ml, W: dry weight of adsorbent in g. The

adsorption results and the equilibrium concentrations of the copper ion were subjected to linear formulas of the Langmuir single-surface equation in order to obtain the adsorption adsorption criteria (maximum capacity, binding capacity, maximum regulatory capacity, regulatory capacity at equilibrium, free energy and preference factor.  $X = \frac{KbC}{(1 + KC)} \dots (2)$ 

Where:

X: the amount of copper adsorbed in  $\mu g g^{-1}$  soil, C: represents the copper concentration in the equilibrium solution in  $\mu g ml^{-1}$ , and b: represents the maximum adsorption in  $\mu g g^{-1}$  and K: the binding factor of the element on the soil surface. energy coefficient in ml  $\mu g^{-1}$ unit.

The values of constants are calculated after plotting the relationship between C / X values and C values to get a straight line, so the slope of the line is 1/b, and the intersection with the y-axis Intercept is 1/Kb.

$$\frac{C}{X} = \frac{1}{Kb + C/b} \dots (3)$$

### Maximum Buffering Capacity (MBC)

This value is expressed mathematically by multiplying the maximum adsorption capacity of the surface (Xm) in the binding energy (K) of the Langmuir equation, which is a characteristic of ion adsorption. The Langmuir equation, as noted by Yassen & Fakher (20) and Al-Hassoon *et al.* (4,5), are as follows:

$$MBC = \frac{dx}{dc} = (K Xm) \dots (4)$$

### **Equilibrium Buffering Capacity (EBC)**

It expresses the gradient of the adsorption curve when the ion concentration in the solution approaches a certain concentration, and is mathematically represented by the tangent slope of the adsorption curve at this concentration in the Langmuir equation.

$$EBC = \frac{KXm}{(1+KC)^2} \dots (5)$$

Thermodynamic parameters

The preference coefficient (separation) (RL) was calculated from the following equation:

$$R_{L} = \frac{1}{(1 + K_{L})C_{0}} \dots (6)$$

where:

 $K_L$  = binding energy, and  $C_0$  = copper concentration in the equilibrium solution.

The Preference Factor  $(\Delta G)$  was calculated from the following equation (Woodruff Equation :

$$\Delta \mathbf{G} = -\mathbf{RT} \ln \mathbf{K} \dots (\mathbf{7})$$

where:

 $\Delta$ G: free energy (kJ mol<sup>-1</sup> kelvin<sup>-1</sup>), R: constant gases, T: absolute temperature (kelvin), K: binding energy.

### **RESULTS AND DISCUSSION**

Results in Table 3 indicate the effect of the concentration of the primary copper ion added concentration in the dvnamic and its equilibrium solution in plant waste (compost), sludge and bentonite metal. This table shows that there is a steady increase in the amount of copper in the equilibrium solution with the added primary concentration. Average concentration copper of followed the arrangement of :

Sludge > Plant waste > Bentonite

The reason for the low concentration of copper balanced with bentonite is due to the high capacity of this metal in the adsorption of copper because it has a large surface area working to draw the largest amount of added concentration and thus the reduction of residual (18).

Primary Copper added	Copper concentration in dynamic equilibrium solution µg ml <sup>-1</sup>			
μg ml <sup>-1</sup>	Plant waste	Sludge	Bentonite	
60	0.2146	0.4986	0.0584	
80	0.2960	0.5947	0.0649	
100	0.3626	0.7487	0.0766	
120	0.6756	0.8957	0.0881	
140	0.7007	1.065	0.0922	
180	0.7990	1.2228	0.1004	
Aevrage	0.5081	0.8376	0.0801	

 Table 3. Copper Concentration in Dynamic Equilibrium Solution

# Effect of the initial concentration of copper ion on the amount adsorption

The results show in table 4 reveal that the adsorption of the adsorbent increased with the concentration of the added Copper solution. This indicates that there are a large number of active sites on the surface of the adsorbent

reached 1799.00,1792.01 and 1787.77  $\mu g g^1$ .

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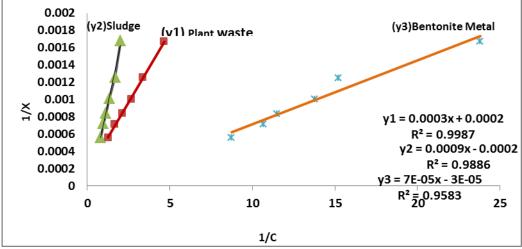
Table 4. Allo	unt of Copper auso	i deu on the mater	lais useu		
Primary Copper added	The amount of Copper adsorbed on the materials used $\ \mu g \ g^{-1}$				
μg ml <sup>-1</sup>	Plant waste	Sludge	Bentonite		
60	597.85	595.01	599.42		
80	797.04	794.05	799.35		
100	996.37	992.51	999.23		
120	1193.24	1191.04	1199.12		
140	1392.99	1389.35	1399.08		
180	1792.01	1787.77	1799.00		
Average	1128.25	1124.96	1132.53		

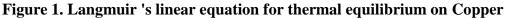
# Table 4. Amount of Copper adsorbed on the materials used

### **Study of thermal equilibrium**

The study of thermal equilibrium of the adsorption process is important to understand how the dissolved material is linked to the adsorbent in order to determine the best

conditions in which the substance is adsorbed. Copper grabs and retains more in plant waste and Bentonite due to the high affinity of Copper to adsorped on its compared with sludge





The Langmuir equation assumes that the maximum adsorption occurs when the primary layer is saturated with solute ions. Constants are as follows: The highest binding capacity of sludge was  $4.5 \ \mu g \ g^{-1}$ , the maximum adsorption capacity of Bentonite 2000000  $\mu g$ 

 $g^{-1}$ . is shown in table 5, and the highest determination coefficient ( $R^2$ ) for plant waste was 1.00, as shown in Figure 1, but generally represents good linear relationship to sludge and Bentonite as well (2).

Table 5. Thermal equilibrium constants in the Langmuir equation for Copper adsorption on
Plant waste, sludge and Bentonite

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Tre.	Bonding energy ml µg <sup>-1</sup>	Maximum adsorption $\mu g g^{-1}(X_m)$	determination coefficient R <sup>2</sup>
Plant waste	1.5	3333.33	1.00
Sludge	4.5	1111.11	0.99
Bentonite	0.0001	2000000	0.96

Maximum regulatory capacity (MBC) and regulatory capacity at balance (EBC) : Table 6 shows the maximum regulatory capacity and the regulatory capacity at equilibrium for Copper. The maximum regulatory capacity values for plant waste, sludge and Bentonite were 4999.995, 4999.995 and 200 ml  $\mu g^{-1}$  respectively. Regulatory capacity values for plant waste, sludge and Bentonite were 1610.216, 218.818 and 200 µg  $g^{-1}$  respectively. The difference in the regulatory capacity values between the adsorbents is due to the different adsorption nature of Copper, and the variation of the maximum adsorption values and the binding energy at the high energy sites caused the ion readiness difference at the different locations of the adsorption curve, as copper adsorption does not differ in nature on all adsorbent surfaces, but the difference is in the nature of the adsorbent surface. The binding of the ion in such materials clearly means that it is easily released from the adsorption surfaces into the solution, causing increased diffusion rates of this ion and subsequent increased absorption by the plant (7). Li et al. (9) explained the importance of MBC values in describing soil contamination by Lead and other heavy metals and that increasing their values indicates that the ionic adsorbent type of the heavy element has a low binding capacity, which facilitates its movement and migration (Heavy Metals Migration) towards the depths of the soil and on the type of heavy element and its movement in the soil.. The soil has a selfpurification capacity and high regulation capacity to cope with pollution.

# Thermodynamic standards

The main advantage of Langmuir equation is to calculate the preference constant ( RL), which can be calculated from the equation, as its value gives a good indication of the nature and form of adsorption. If its value is greater than 1, this indicates that adsorption is not preferred, and adsorption is linear if its value is 1, and adsorption is preferred if its value is between 0-1, and adsorption is not reversed if its value is 0. Through this study and by applying Langmuir equation, it was found that the value of the preference coefficient constant for plant residues, sludge and Bentonite 0.78, 0.22, 12.50, respectively, which indicates that adsorption is preferable and non-reversible for plant residues and sludge, unfavorable and inverse for Bentonite for the studied system. . Table 6 also shows that the adsorption reactions were spontaneous with Bentonite, indicating that the free energy value was negative and that the reaction was negative while the free energy values of Copper adsorption of plant waste and sludge were shown. It clearly shows that this reaction is not automatic and requires additional activation energy, and that these values are in line with the values of the preference factor (separation coefficient,  $R_L$ ) (20).

		preference	factor	,
Tre.	MBC (ml μg <sup>-1</sup> )	EBC (ml μg <sup>-1</sup> )	ΔG KJ mol <sup>-1</sup> Kelvin <sup>-1</sup>	R <sub>L</sub>
Plant waste	4999.995	1610.216	0.06	0.78
Sludge	4999.995	218.818	0.21	0.22
Bentonite	200	200	-1.30	12.48

Table 6. Maximum regulatory capacity, regulatory capacity at equilibrium, free energy and

## Achnowledhment

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